



NORWEGIAN CCS RESEARCH CENTRE

## Task 9 Webinar: Fault integrity screening

Webinar, 17 Nov 2018

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# 3D fault integrity screening for Smeaheia CO<sub>2</sub> injection site

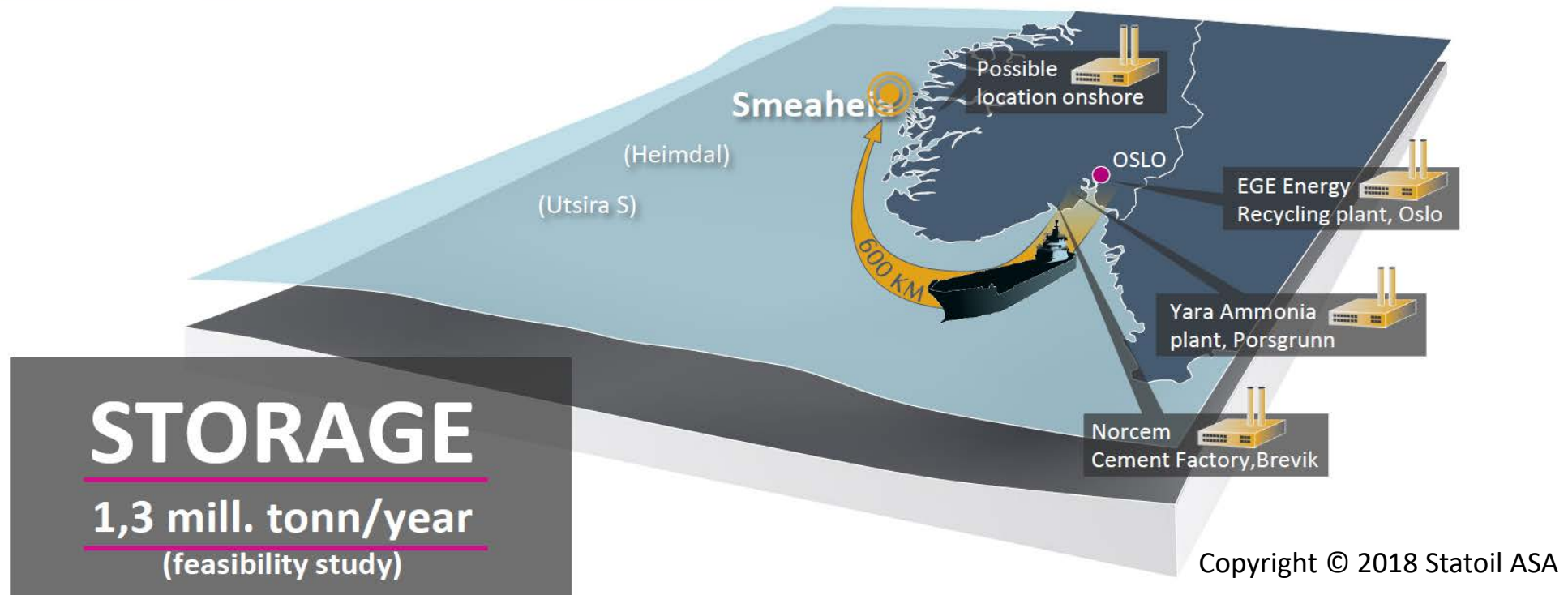
NCCS TASK 9 WEBINAR

## Improved fault risk workflow in task 9



# Norwegian full scale CCS demonstration

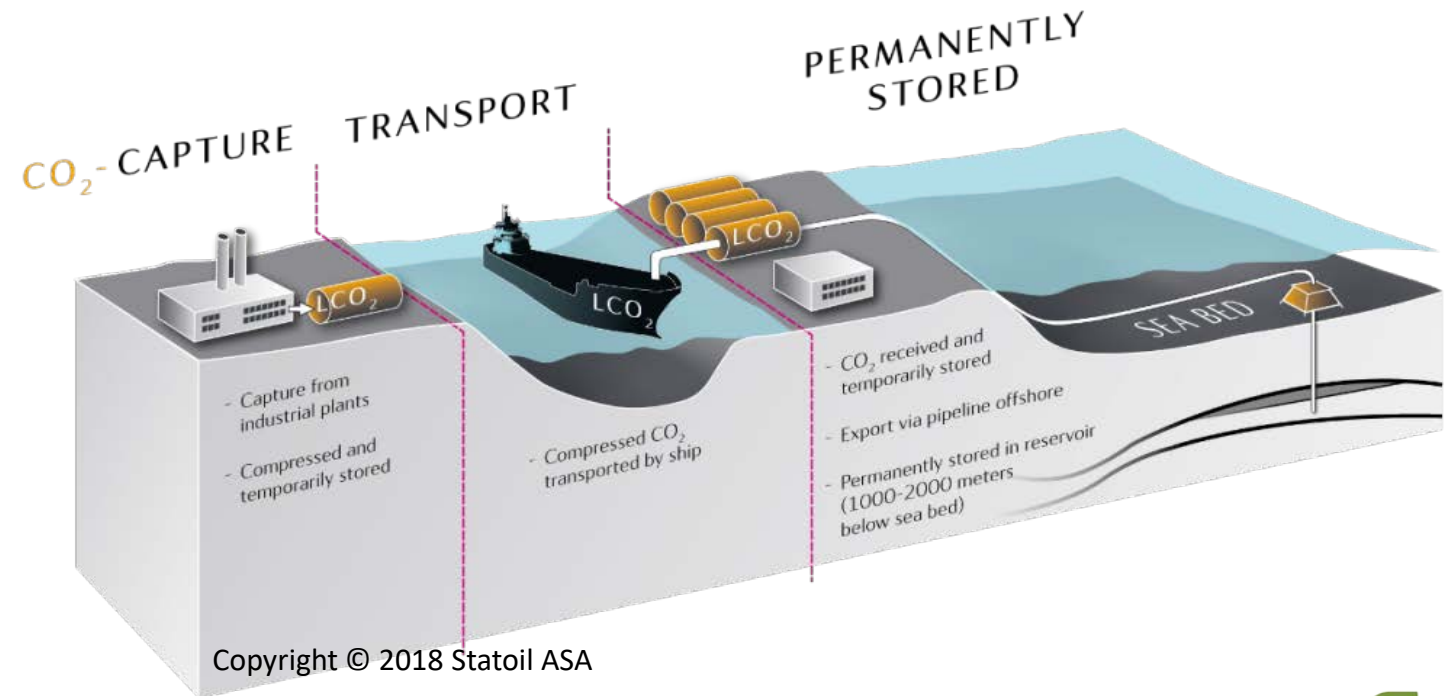
Feasibility study



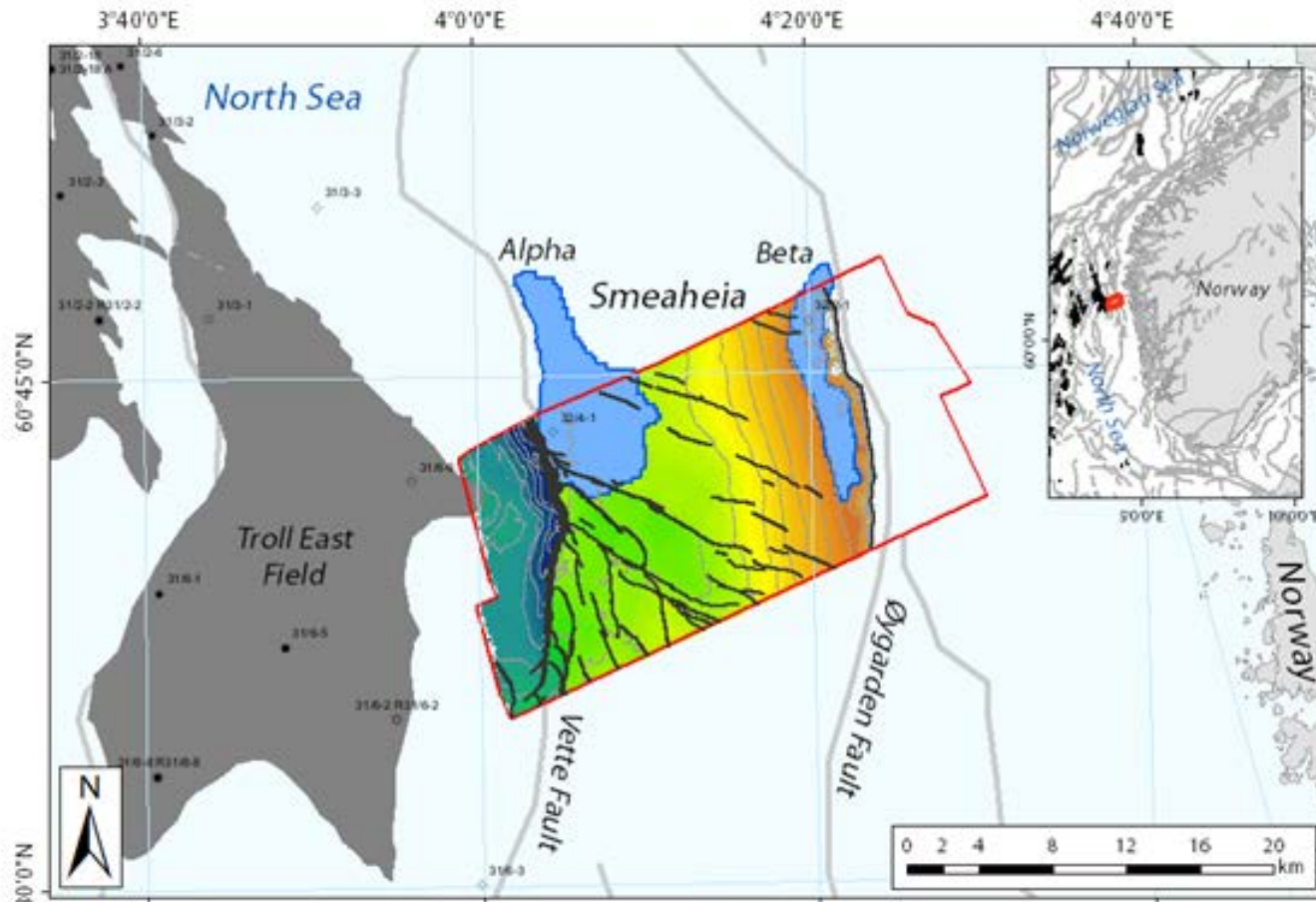
# Northern Lights project

## – Equinor (former Statoil), Total, Shell

- Smeaheia suggested storage site offshore western Norway
- Johansen Fm, Aurora site, south of Troll selected for further investigation



# Location



## Legend

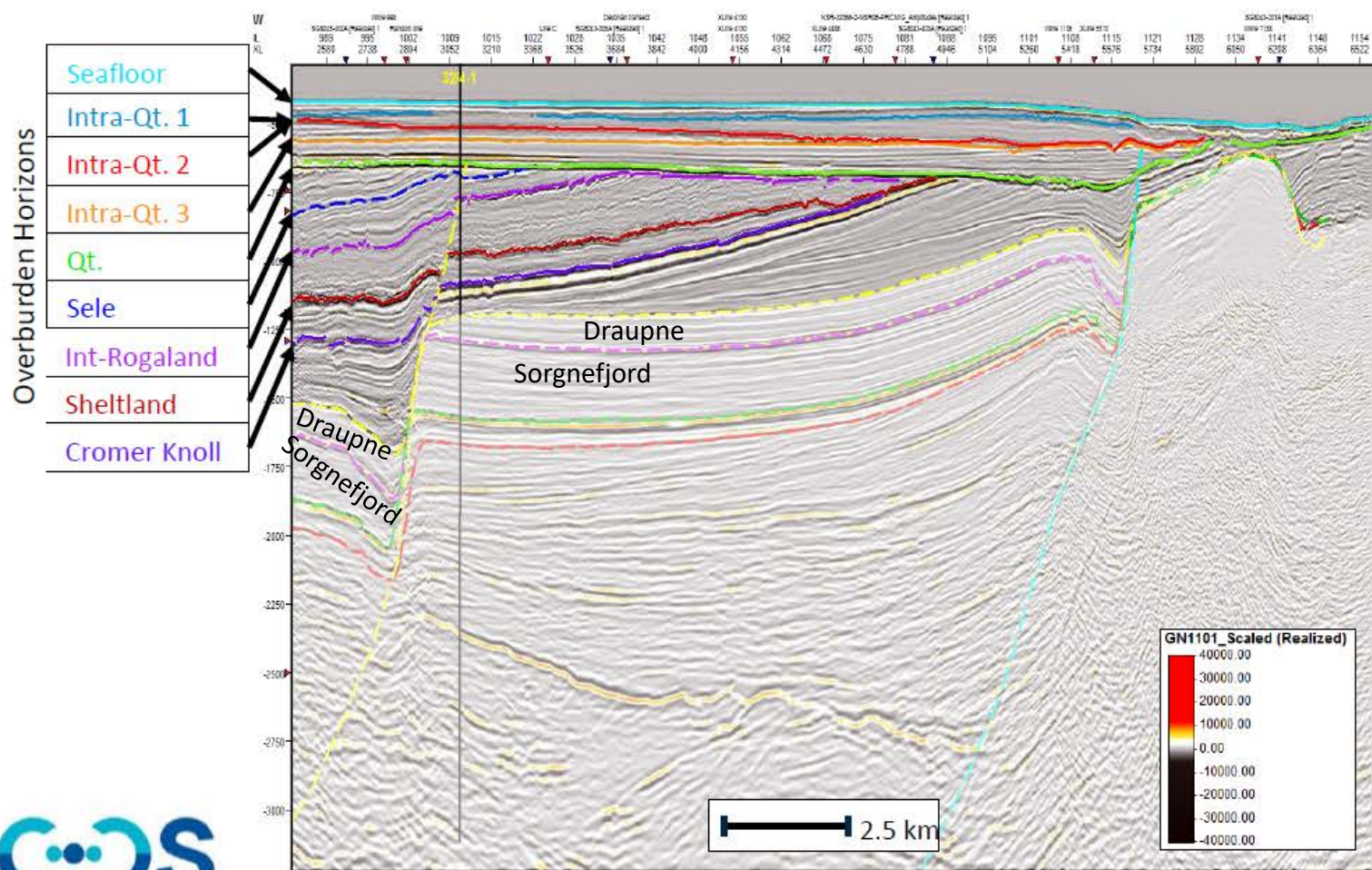
- |                            |                       |  |
|----------------------------|-----------------------|--|
| GN1101 3D Seismic Data     | Exploration Wellbores | <b>Top Sognefjord Structure (m s TWT)</b><br>940<br><br>1870<br>Contour Interval: 50 |
| Hydrocarbon Fields         | Regional Faults       |  |
| Smeaheia Prospect Closures | Analyzed Faults       |  |

- Data:

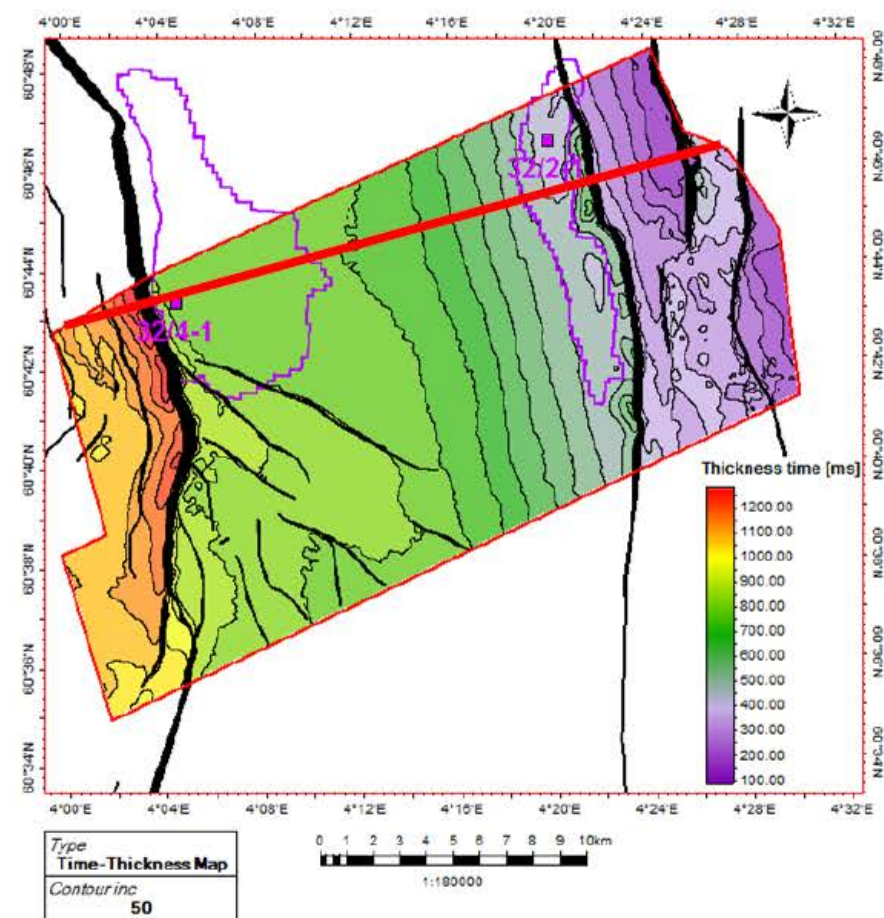
- Seismic
- Two wells in Smeaheia/logs
- Core from Sognefjord/Heather
- Toll/Troll East, as an analogue
- Data package, Smeaheia

# Geology

- Seismic interpretation



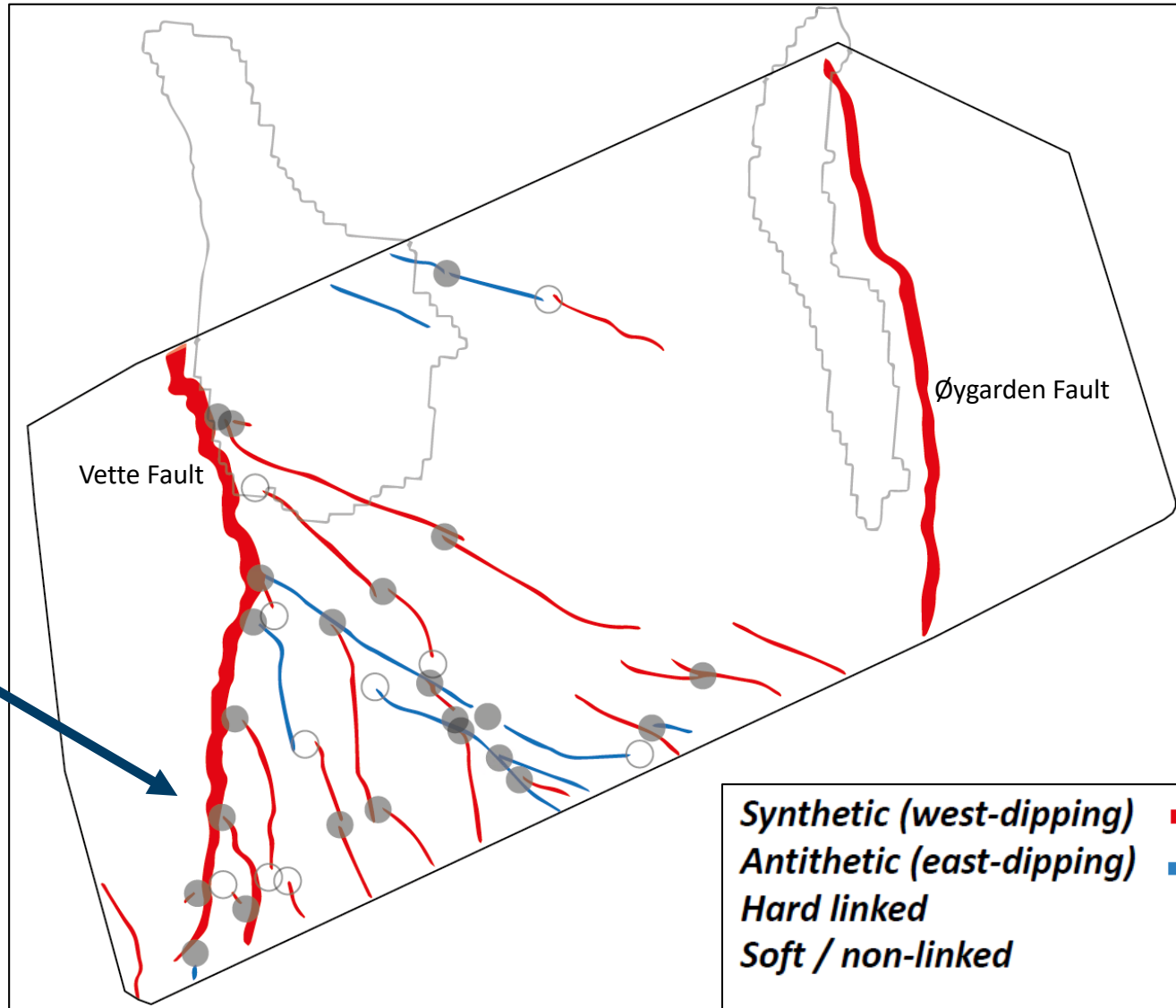
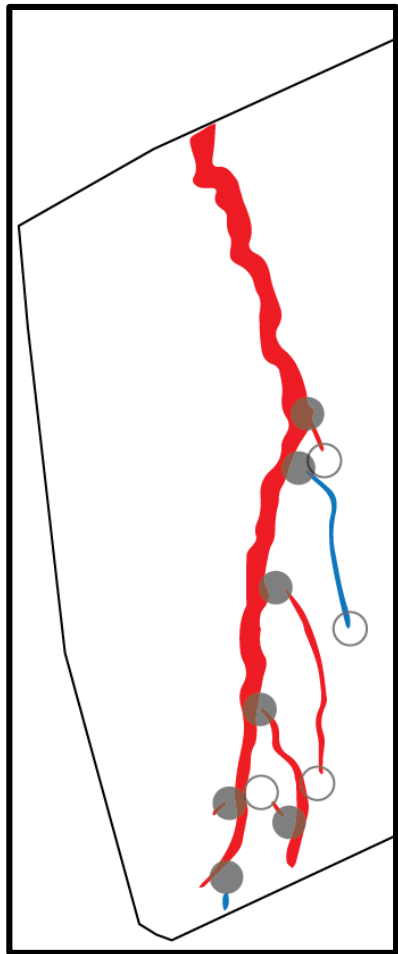
Top Draupne to Seafloor: Overburden Isochron (ms TWT)



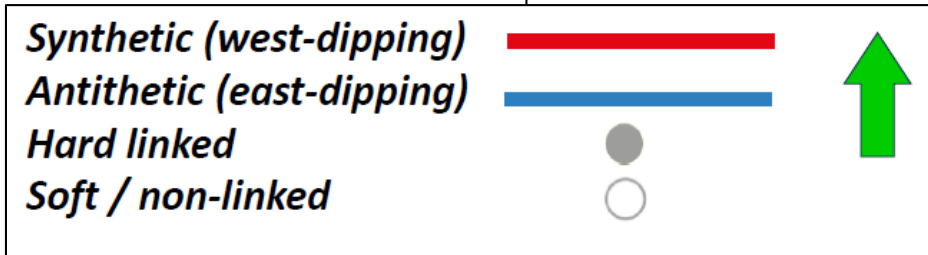
V.E. = 5



# Identified risk aspects reservoir



Top Sognefjord





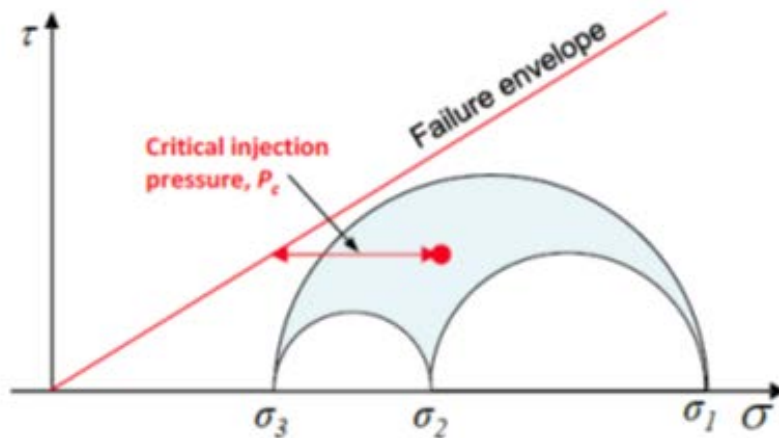
# Motivation

- Mature the Smeaheia fault seal system understanding
- Reduce the risk related to CO<sub>2</sub> injection in faulted reservoirs

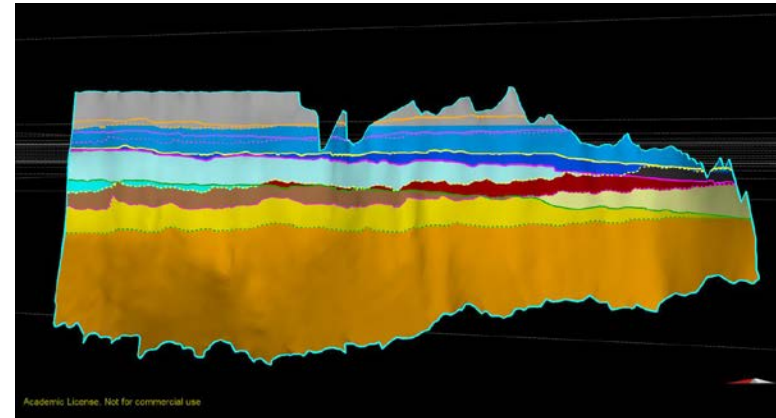
# Models for fault seal integrity

- 3D screening of fault slip stability
  - stress distribution on slip surfaces

- Fault seal capacity
  - Juxtaposition
  - Clay content

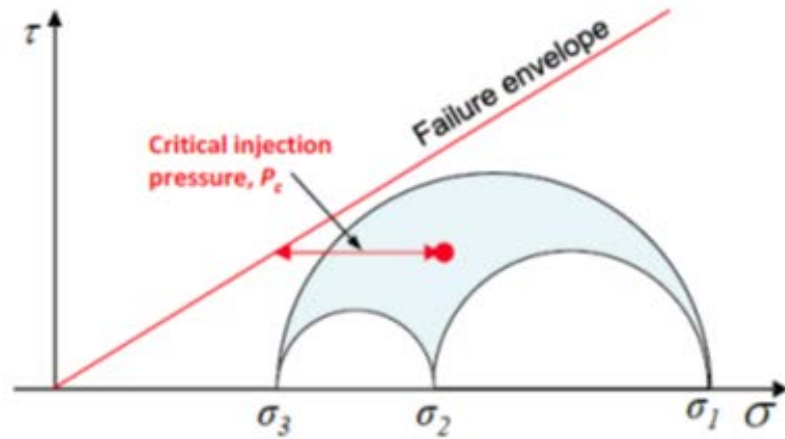


+



- ➔ Detailed geomechanical model
- ➔ Coupled hydro-mechanical model

# 3D screening of fault slip stability

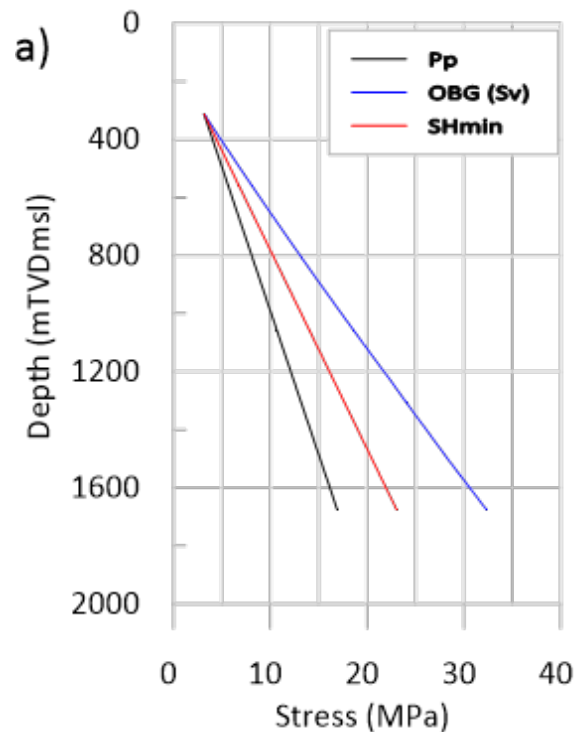


$$\tau_s = c + \sigma_n \tan \phi$$

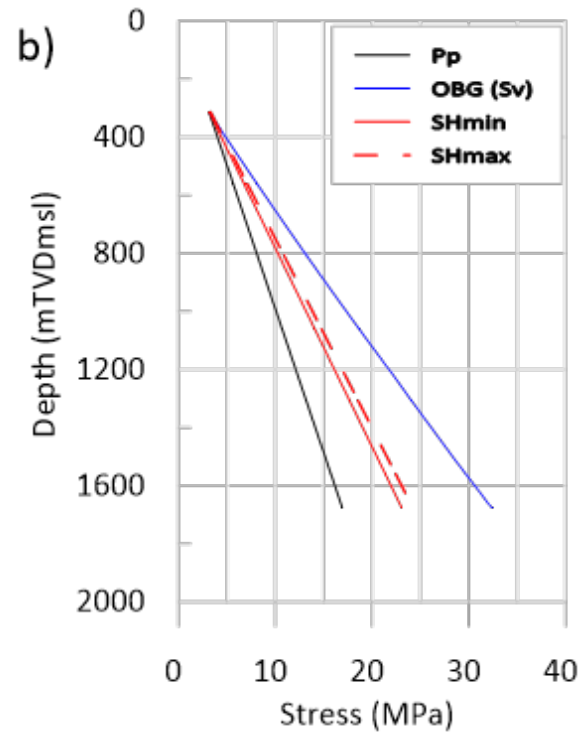
- Simple model considering
  - Stress distribution
  - Material strength/failure criteria
  - Fault geometry
  - Deformation/strain not included
  - Assuming same pressure conditions on the fault as in the reservoir

# Stress distribution – North Sea

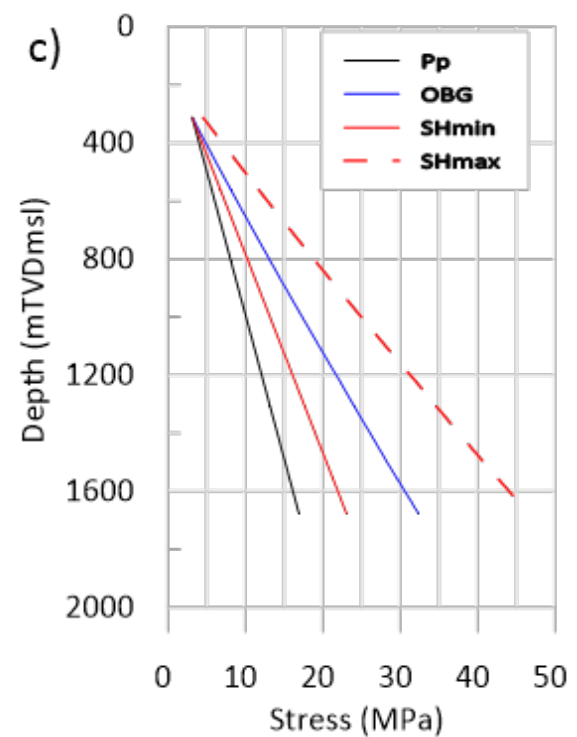
Normal faulting regime  
-isotropic ( $S_H \sim S_h$ )



Normal faulting regime  
-anisotropic ( $S_H$  5% more than  $S_h$ )



Strike-slip regime  
( $S_H > OBG$ )



OBG and Shmin, Equinor Smeaheia data package

# Material properties and fault strength

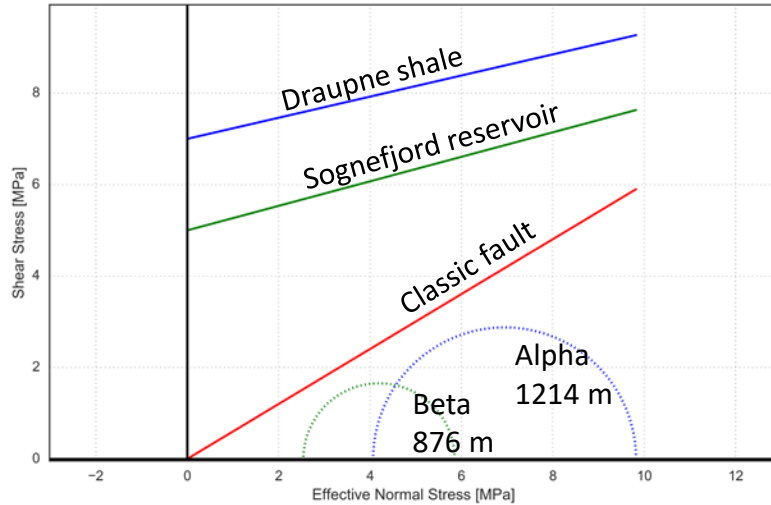
- Well logs – only two available in Smeaheia
- Core tests – limited from Smeaheia, data from Troll/nearby areas

Material	Cohesion (MPa)	Friction angle (deg)	Friction coefficient
Sognefjord, reservoir	5	15	0.27
Draupne, top seal	7	13	0.23
Static friction faults	0	31	0.6

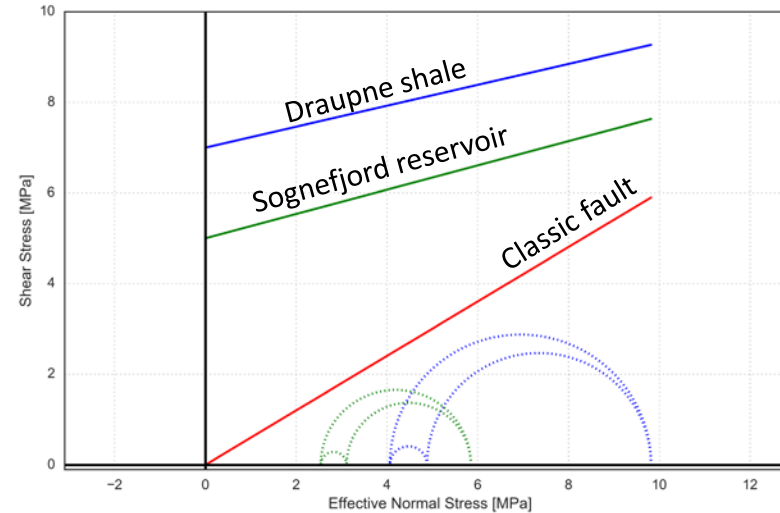
Equinor Smeaheia datapackage, average values

# Fault stability –screening, *in situ* conditions

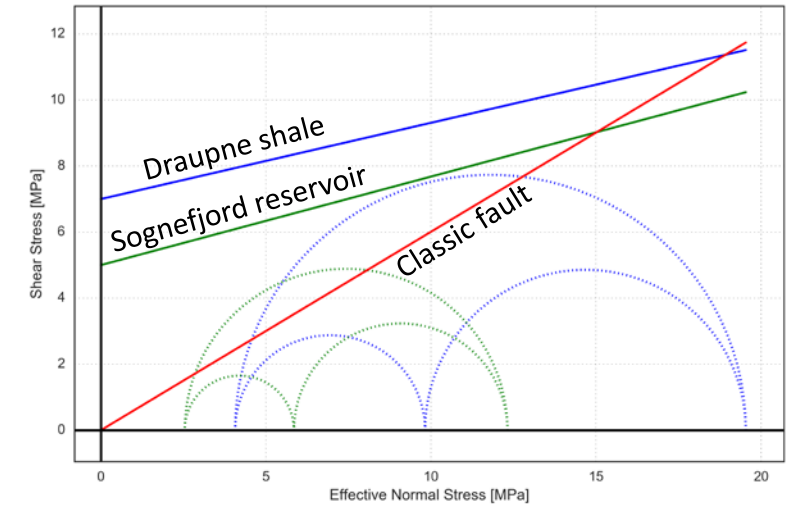
Normal faulting regime  
-isotropic ( $S_H \sim S_h$ )



Normal faulting regime  
-anisotropic ( $S_H$  5% more than  $S_h$ )



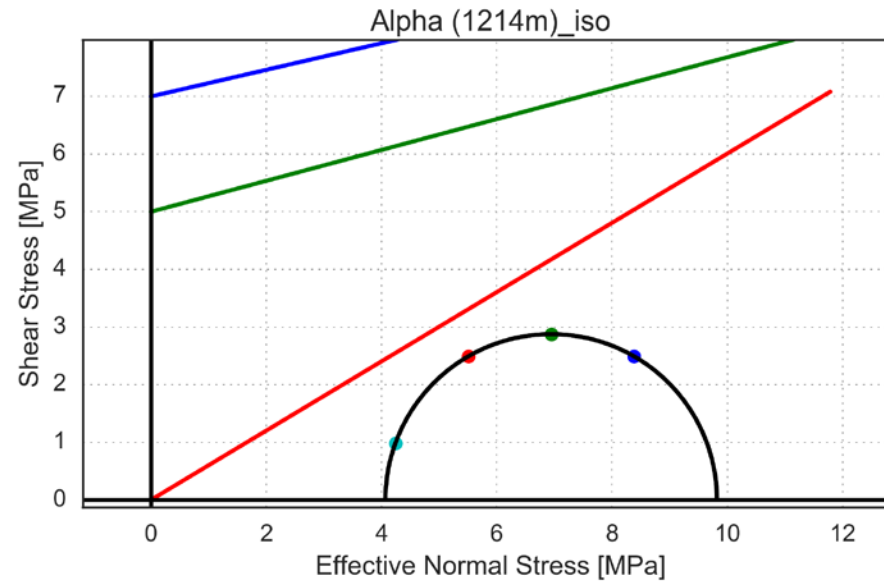
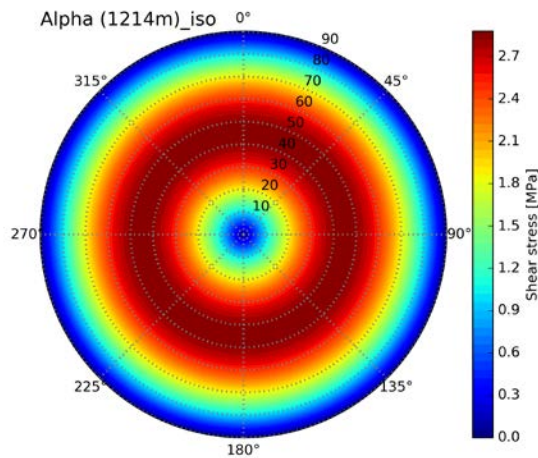
Strike-slip regime  
( $S_H > OBG$ )



Injection  $\leftarrow \rightarrow$  Depletion = reduced risk

- Anisotropy – favorable orientation more stable
- Non-cohesion faults - risk for shear failure during pp increase
- Material cohesion included in model = tensile failure risk during pp increase

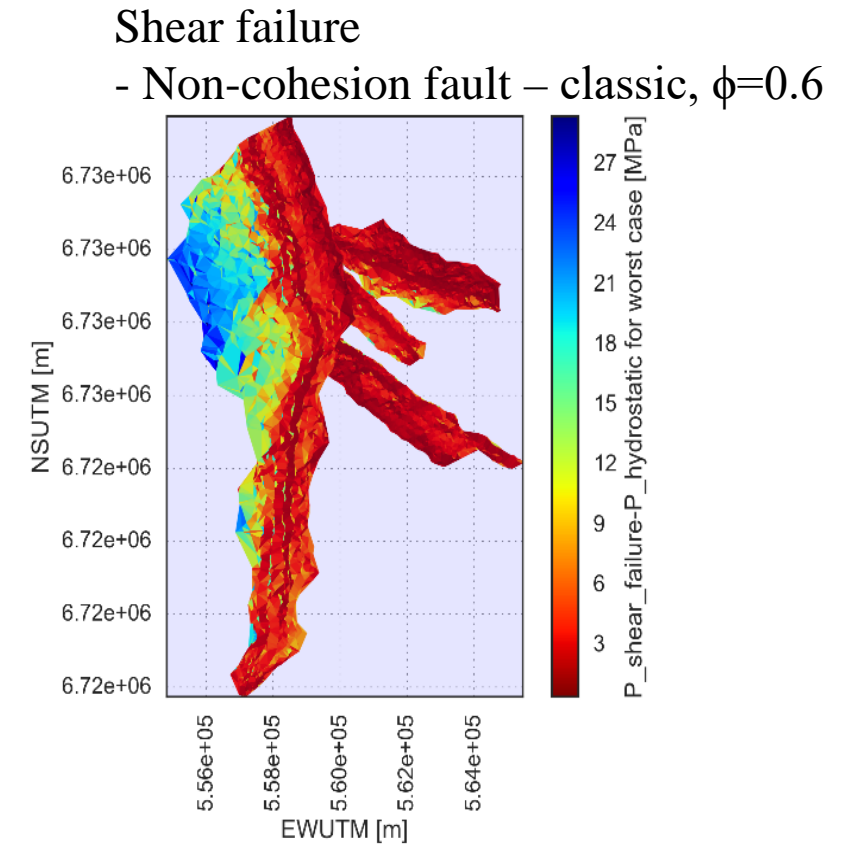
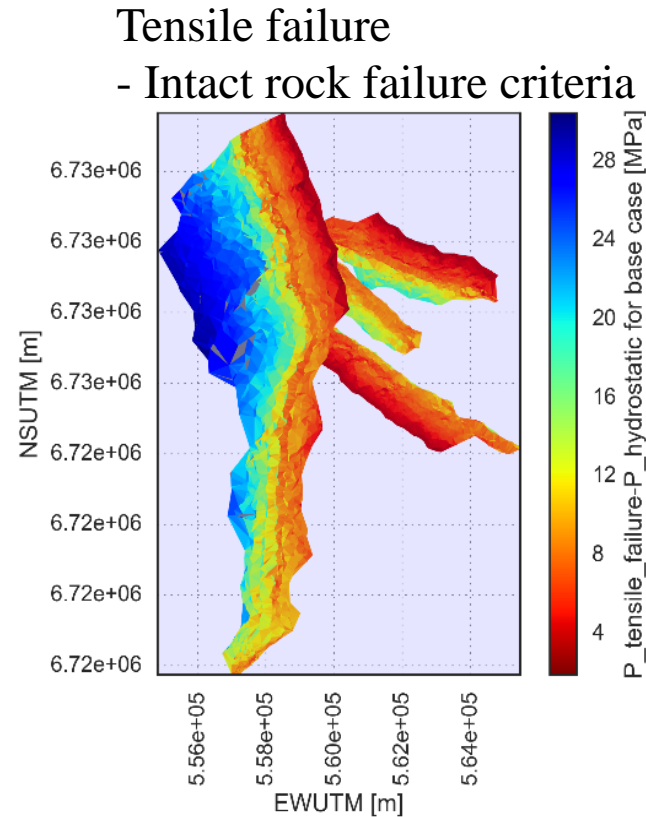
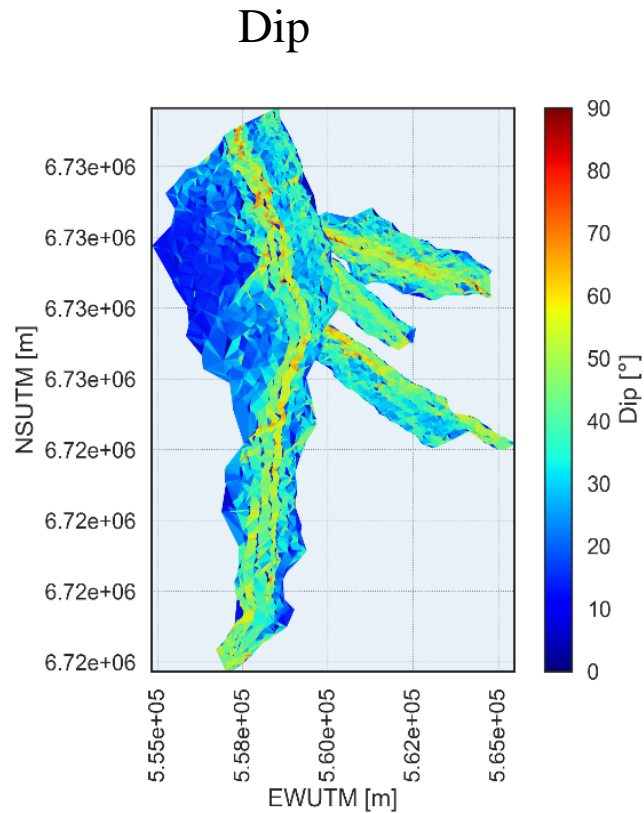
# Fault stability - dip



- Draupne Shale:  $c = 7.0$  MPa,  $\phi = 13.0^\circ$
- Sognefjord Reservoir:  $c = 5.0$  MPa,  $\phi = 15.0^\circ$
- Classic fault:  $c = 0.0$  MPa,  $\phi = 31.0^\circ$
- Strike =  $170.0^\circ$ , Dip =  $30.0^\circ$
- Strike =  $170.0^\circ$ , Dip =  $45.0^\circ$
- Strike =  $170.0^\circ$ , Dip =  $60.0^\circ$
- Strike =  $170.0^\circ$ , Dip =  $80.0^\circ$

- Highest shear stress on  $45^\circ$
- Most critical for shear failure:  $60^\circ$
- Most critical for tensile failure:  $80-90^\circ$

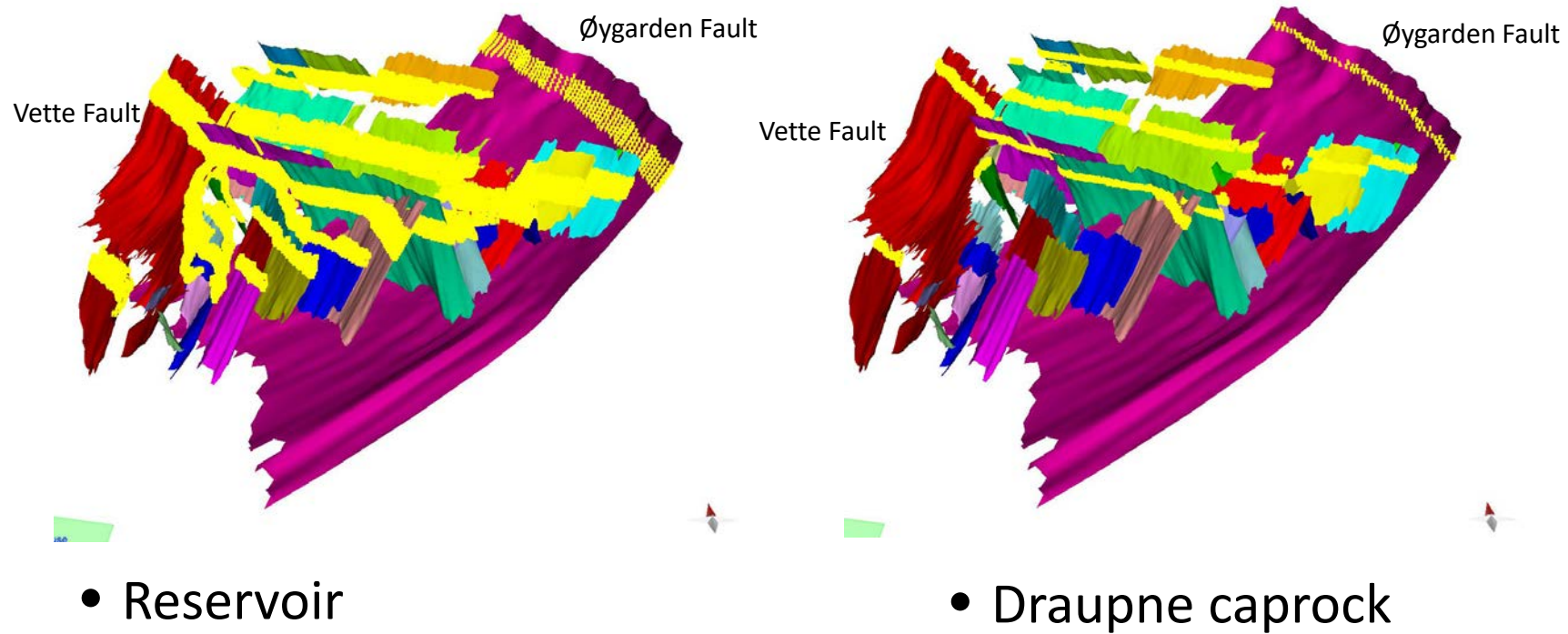
# 3D screening on selected faults



- Tool to get the overview
- Problems:
  - Different failure criteria (frictional stability) for reservoir and seal
  - Pp increase only relevant for reservoir section

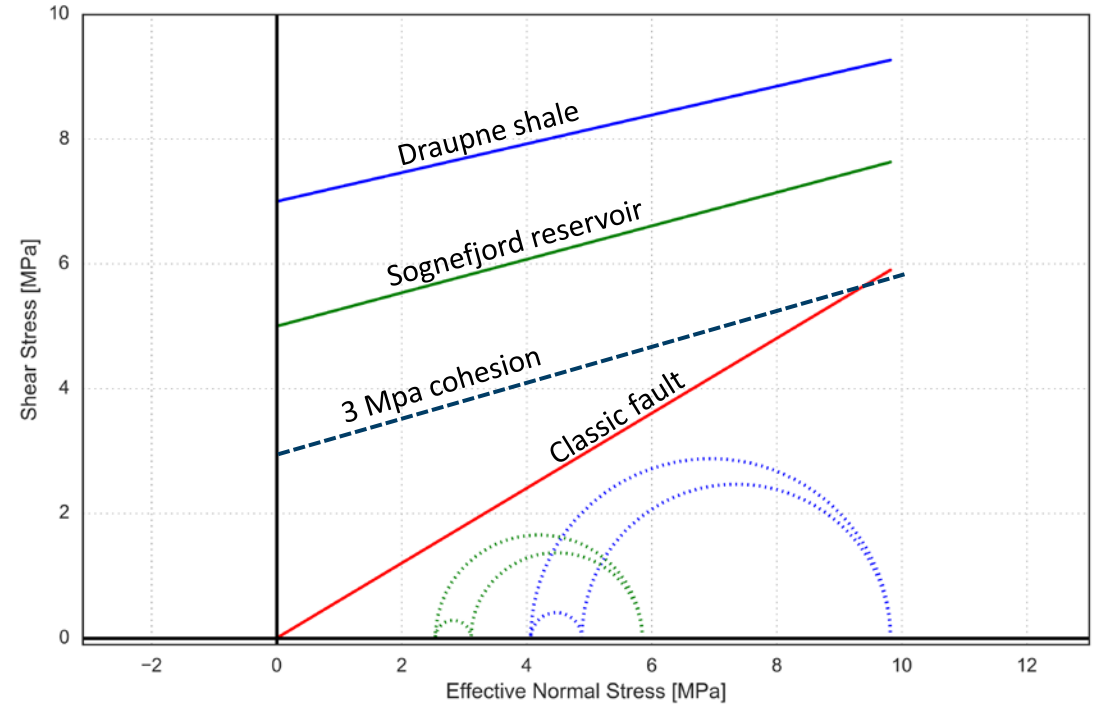


# Refinement of slip stability analysis



# Summary of the 3D fault stability screening

- Classic fault failure criteria:
  - A very limited  $p_p$  increase before the faults will be critically stressed
- Cohesion of 3 MPa on the fault
  - A tensile failure criteria/fracture gradient will apply also for faults

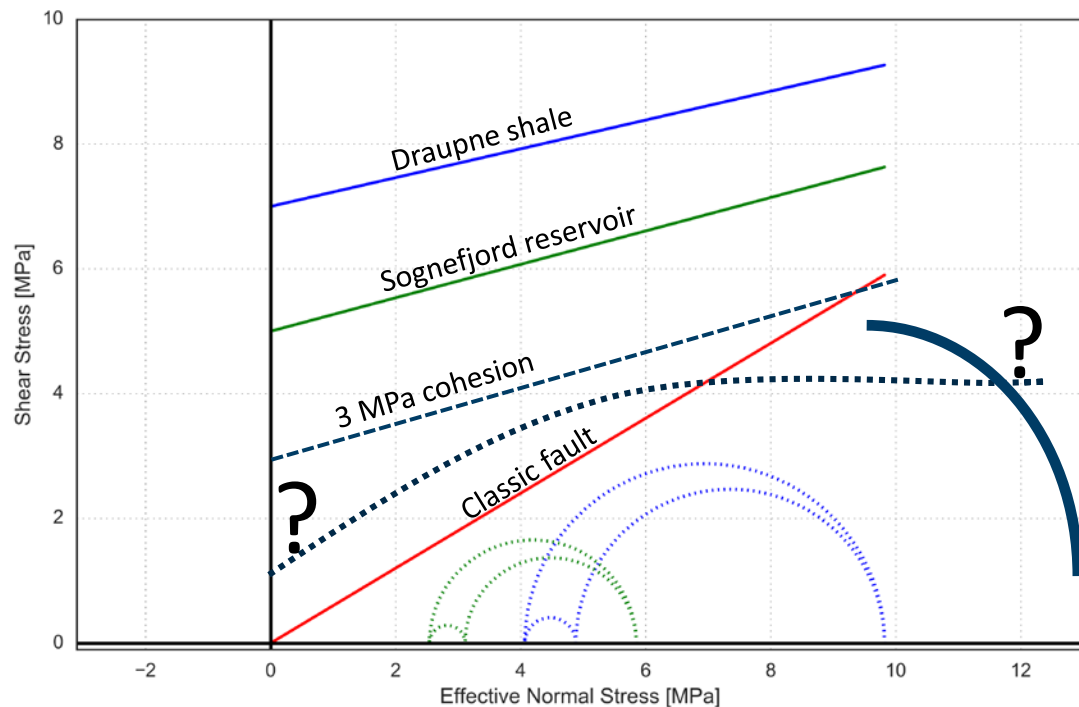


Can cohesion be expected for faults in Sognefjord and Draupne lithology?

How to address / quantify this?

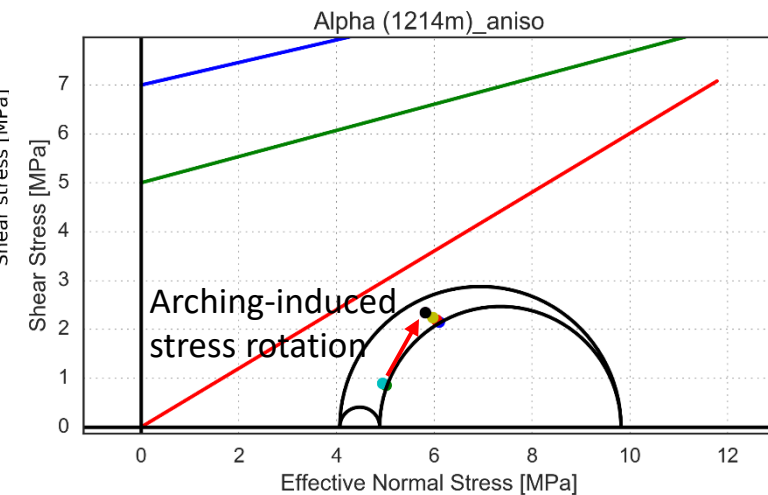
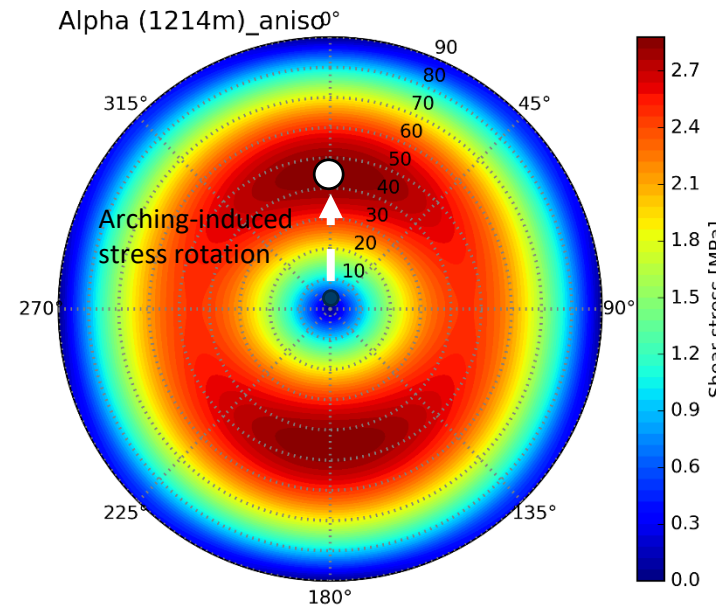
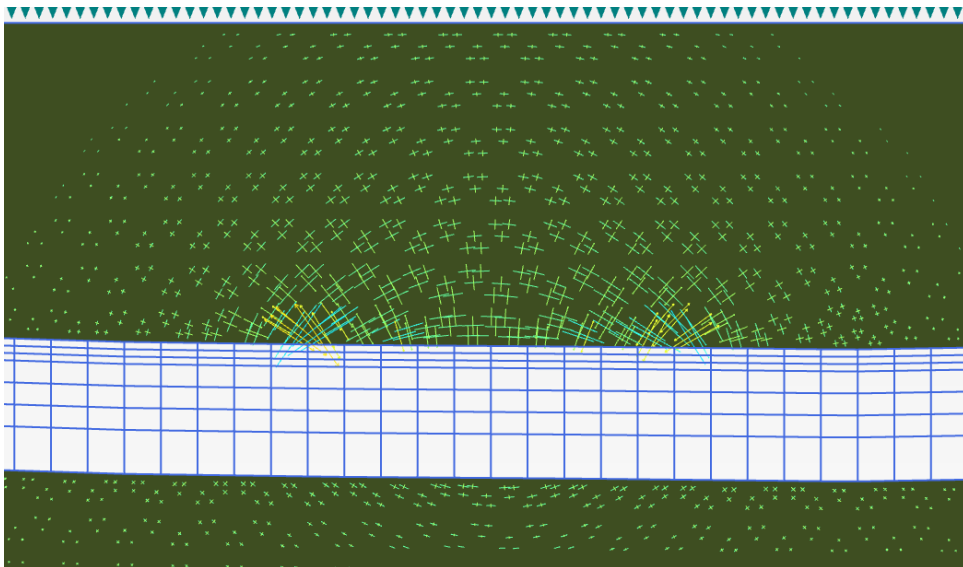
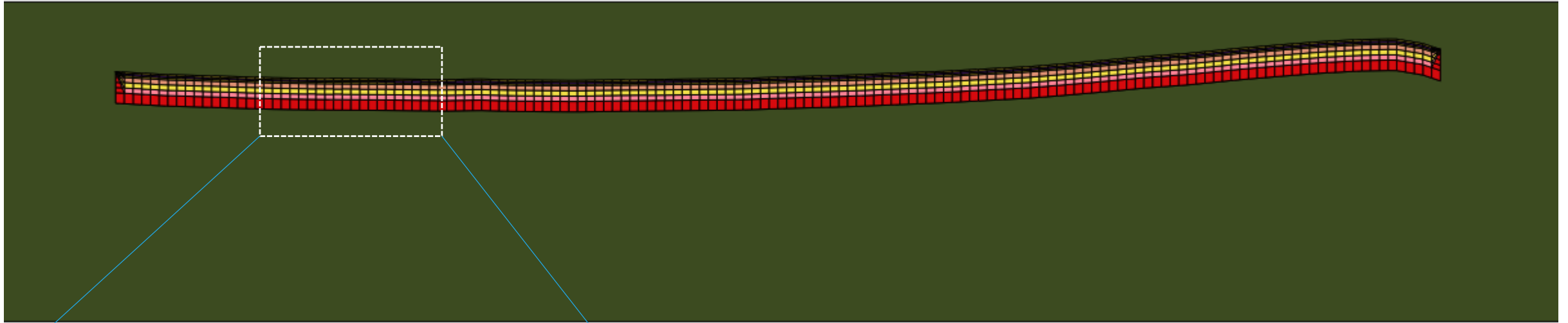
How about overburden?

# Continuation of work in task 9



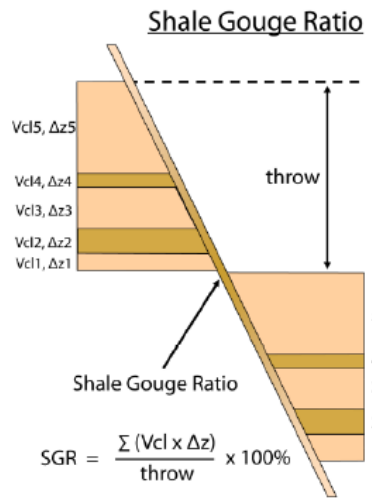
- Material properties /material behavior during Pp changes
  - Sognefjord, Draupne, Cromer Knoll/Shetland, Heather (mixed zones in faults?)
- Stress path vs Strain/deformation in overburden/along faults
  - Arching effects, fault drainage conditions/temperature
- Juxtaposition/seal
  - Uncertainty in Cromer Knoll and Shetland flow properties
- Fault growth – and history

# Impact of Arching-induced Stress Rotation in Overburden on Shear Slip Tendency



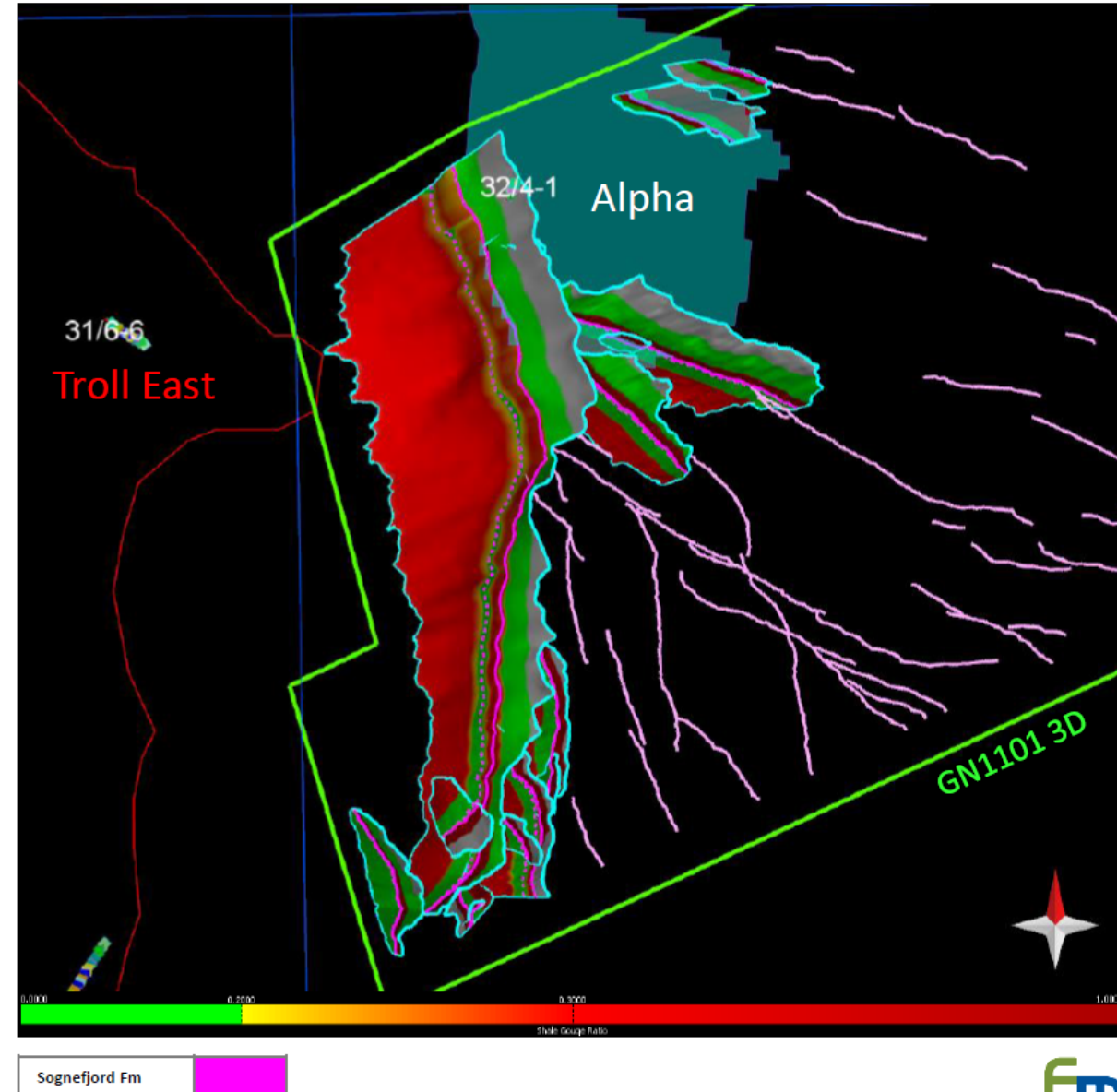
# Shale Gouge Ratio Model

- Shetland and Cromer Knoll treated as clay-free carbonate intervals ( $0.0 V_{sh}$ )
- Interval  $V_{sh}$  based on lithology, log-based SGR will be undertaken later and calibrated using Tusse fault results from Troll East
- Calculations limited to fault cutoffs



Redrawn from Yielding et al., 2010

Horizon	Color	Lithology	$V_{sh}$
Shetland Gp	Orange	Marl	0.0
Cromer Knoll Gp	Purple	Marl	0.0
Draupne Fm	Yellow	Mudstone	1.0
Sognefjord Fm	Pink	Sandstone	0.0
Brent Gp	Green	Siltstone	0.5



# Thanks for you attention

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